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for

**REDUCTION OF INTERFERENCE PICKUP IN HEADS FOR
MAGNETIC RECORDING BY MINIMIZING PARASITIC
CAPACITANCE**

REDUCTION OF INTERFERENCE PICKUP IN THE HEADS FOR MAGNETIC RECORDING BY MINIMIZING PARASITIC CAPACITANCE

BACKGROUND OF THE INVENTION

1. The Field of the Invention

The invention relates generally to magnetic storage devices. More specifically, the present invention relates to disk drives where data is stored on and retrieved from magnetic media using a read/write head.

2. The Relevant Art

Computer systems generally utilize auxiliary memory storage devices having media on which data can be written and from which data can be read for later use. A direct access storage device, such as a disk drive, incorporating rotating magnetic disks is commonly used for storing data in magnetic form on the disk surfaces. Data is recorded on concentric, radially spaced tracks on the disk surfaces. Magnetic heads carrying read sensors are then used to read data from the tracks on the disk surfaces.

In high capacity disk drives, magnetoresistive read sensors, commonly referred to as MR heads, are commonly used. This is largely due to the capability of MR heads of reading data on a disk of a greater linear density than that which the previously used thin film inductive heads are capable of. An MR sensor detects a magnetic field through a change in resistance in its MR sensing layer (also referred to as an "MR element") as a function of the strength and direction of the magnetic flux being sensed by the MR layer.

The conventional MR sensor operates on the basis of the anisotropic magnetoresistive (AMR) effect in which an MR element resistance varies as the square of the cosine of the angle between the magnetization of the MR element and the direction of sense current flowing through the MR element. Recorded data can be read from a magnetic medium because the external magnetic field from the recorded magnetic medium (the signal field) causes a change in the direction of magnetization in the MR element, which in turn

causes a change in resistance in the MR element and a corresponding change in the sensed current or voltage.

Another recently developed type of MR sensor is the giant magnetoresistance (GMR) sensor manifesting the GMR effect. In GMR sensors, the resistance of the MR sensing layer varies as a function of the spin-dependent transmission of the conduction electrons between magnetic layers separated by a non-magnetic layer (spacer) and the accompanying spin-dependent scattering which takes place at the interface of the magnetic and non-magnetic layers and within the magnetic layers.

GMR sensors using only two layers of ferromagnetic material separated by a layer of non-magnetic electrically conductive material are generally referred to as spin valve (SV) sensors manifesting the GMR effect. In an SV sensor, one of the ferromagnetic layers, referred to as the pinned layer, has its magnetization typically pinned by exchange coupling with an antiferromagnetic (e.g., NiO or Fe-Mn) layer.

The magnetization of the other ferromagnetic layer, referred to as the free layer, however, is not fixed and is free to rotate in response to the field from the recorded magnetic medium (the signal field). In SV sensors, the SV effect varies as the cosine of the angle between the magnetization of the pinned layer and the magnetization of the free layer. Recorded data can be read from a magnetic medium because the external magnetic field from the recorded magnetic medium causes a change in the direction of magnetization in the free layer, which in turn causes a change in resistance of the SV sensor and a corresponding change in the sensed current or voltage. It should be noted that the AMR effect is also present in the SV sensor free layer and it tends to reduce the overall GMR effect.

The disk drive industry has been engaged in an ongoing effort to increase the overall GMR effect while maintaining the highest signal-to-noise ratio possible. As the size of components in the disk drive industry become smaller and more compact, the possibility of noise interference increases dramatically. Prior art disk drives and recent industry efforts have failed to develop adequate methods of increasing the signal-to-noise ratio.

1 Therefore, it should be apparent that a need exists for a method of minimizing the
2 amount of noise interference present in a disk drive system, thus maximizing the level of
3 signal received.
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EXHIBIT 100

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In a further embodiment, the reduced capacitance disk drive head comprises a stud that is formed through the low dielectric material. The use of the low dielectric material is configured to decrease the parasitic capacitance of the disk drive head. The stud formed through the low dielectric material may comprise the element copper (Cu) or

another electric conducting material. The low dielectric material may be configured to comprise a hard bake photo resist. In one embodiment, the low dielectric material may comprise silicon dioxide (SiO_2). The low dielectric material is preferably configured to have a dielectric constant of less than about nine. In one embodiment, the low dielectric material has a dielectric constant of about three. The low dielectric material may provide a platform for the electrical contact pad. The reduced capacitance disk drive head is configured in one embodiment to carry a GMR sensor.

The reduced capacitance disk drive head may comprise an electrical contact pad, a substrate on which the disk drive head may be formed, and a low dielectric material interposed between the pad and the substrate. The low dielectric material is configured to be a platform for the electrical contact pad to increase the distance between the substrate and the electrical contact pad. The low dielectric material is also configured to comprise hard bake photo resist.

The reduced capacitance disk drive head in a further embodiment comprises a reduced area pad, a reduced area lead, and a substrate on which the disk drive head is formed. In another embodiment, the reduced capacitance disk drive head comprises an electrical contact pad, an alumina undercoat layer comprising Al_2O_3 , a substrate on which the disk drive head is formed, and an additional layer of material interposed between the pad and the aluminum undercoat layer, the additional layer comprising alumina. The reduced capacitance disk drive head may also be configured with an additional layer of material interposed between the pad and the aluminum undercoat layer, the additional layer preferably comprising SiO_2 .

These and other objects, features, and advantages of the present invention will become more fully apparent from the following description and appended claims, or may be learned by the practice of the invention as set forth hereinafter.

BRIEF DESCRIPTION OF THE DRAWINGS

In order that the manner in which the advantages and objects of the invention are obtained will be readily understood, a more particular description of the invention briefly described above will be rendered by reference to specific embodiments thereof which are illustrated in the appended drawings. Understanding that these drawings depict only typical embodiments of the invention and are not therefore to be considered to be limiting of its scope, the invention will be described and explained with additional specificity and detail through the use of the accompanying drawings in which:

Figure 1 is a cross-sectional view illustrating the composition of a disk drive head with a suspension arm and a magnetic media disk of the prior art;

Figure 2 is a cross-sectional view illustrating the composition of a typical prior art disk drive head for magnetic recording;

Figure 3 is a schematic circuit diagram showing the equivalent impedance between the magnetic disk and the suspension arm;

Figure 4 is a chart illustrating the relationship between the RF interference and the resistance from the substrate to the suspension arm;

Figure 5 is a schematic circuit diagram showing the equivalent impedance between the electrical contact pads and the substrate; and

Figure 6 is a cross-sectional view of a disk drive head illustrating the low dielectric material and studs interposed between the electrical contact pads and the alumina undercoat of the present invention.

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frequency noise can propagate into the head by capacitive coupling (C_{D-Sub}) 306 between the disk 302 and the conductive head substrate 318, capacitive coupling (C_{D-S1} , C_{D-S2}) 308 between the magnetic disk 302 and the magnetic shields 314, or capacitive coupling through any other conductor in the head 300 forming a capacitive coupling with the disk surface 302.

Other capacitive coupling discovered by the inventors and depicted in Figure 3 include shield capacitance 310 (C_{S1-S2}) and substrate to shield capacitance 312 (C_{S-S1}). The value of the capacitance is proportional to the area of the conductive element, and is inversely proportional to the separation between the two conductors. The following equation provides a good approximation for calculating the capacitance between the relative conductive surfaces of the different capacitances depicted in Figure 3.

$$C = \epsilon\epsilon_0(\text{Area} / d)$$

(Eq. 1)

Where $\epsilon_0=8.85 \times 10^{-12} \text{ coul}^2/\text{N} \cdot \text{m}^2$, ϵ is the dielectric constant of the separating gap, A is the area, and d is the distance between the conductors. The capacitance values of the capacitors shown in Figure 3 will depend on the head design, including factors like the shield area 314 (S1) at the ABS, fly height, air bearing, etc. For a typical head, the largest capacitance is formed by the conductive slider substrate 306 and the disk 302, with values of the conductive substrate 306 ranging from $C_{D-Sub}=20$ to 500pF . The slider substrate 306 must be well grounded through the suspension 304, and the resistance 316 ($R_{Sub-Susp}$) must be extremely low, so as to prevent most of the electric interference from the disk 302 to be transmitted into the slider 306. From the slider substrate 306, the signal can then propagate into the read element through a number of elements.

Referring now to Figure 4, illustrated therein is the relationship between the RF interference and the resistance from the substrate 318 to the suspension arm 304 of Figure 3.

Figure 4 illustrates the relationship of the interference transmitted into the slider as a function of $R_{Sub-Susp}$ at 100MHz for $C_{D-Sub}=500\text{pF}$ according to the equation:

$$V_{Sub}=V_{Disk}(R_{Sub-Susp} / R_{Sub-Susp} + (1/j\omega C_{D-Sub}))$$

(Eq. 2)

As can be seen from the chart 400, as the value of $R_{\text{Sub-Susp}}$ is increased, the transmitted noise in the head is increased dramatically.

Figure 5 is a schematic circuit 500 showing the equivalent impedance between the electrical contact pads 502 and the substrate 504. As seen in Figure 5, there are numerous capacitances through which the interference, picked-up by the slider substrate 504 can couple into the read element 502. The interference level can be calculated, and in the case of the single-ended amplifier, is given by the following equation:

$$V_{MR} = V_{Sub} \frac{R_{MR}}{R_{MR} + \frac{1}{j\omega C_{MR-Sub}}}$$

(Eq. 3)

In the above mentioned equation, C_{MR-Sub} is given by the equation below, assuming that $R_{\text{SENSOR LEADS}}$ 506, R_{Coil} 508, and R_{MR} 510 are relatively small.

$$C_{MR-Sub} = C_{Sub-R+} + \left(\frac{1}{C_{Sub-S1}} + \frac{1}{C_{S1-K5} + C_{S1-Dp}} \right)^{-1} + \left(\frac{1}{C_{Sub-W-}} + \frac{1}{C_{Coil-Dp+} + \left(\frac{1}{C_{Coil-P1} + C_{Coil-P2}} + \frac{1}{C_{P1-K5+}} \right)^{-1}} \right)^{-1}$$

(Eq. 4)

In equation 4, the capacitance 512 indicated by the term, C_{Sub-R+} is the contribution from coupling between the read pads 502 and the substrate 504. Further capacitances 514, 516, and 518, indicated by the terms C_{Sub-S1} and $C_{S1-SENSOR LEADS}$, and C_{S1-Dp} respectively, result from coupling through the write pads 502 into the coil 508 and from shields into MR leads. The highest contributors to the capacitive pickup are the magnetic shield 1(S1) 314, (of Figure 3) and the MR pads 510, while coupling through the coil 508 has a second order effect. For a typical head design, the calculated voltage, picked up into the read element 502 of the head 500, constitute 1-5% of the interference present in the drive 500.

Figure 6 is a cross-sectional view of a typical disk drive head 600 illustrating several manners under the present invention of reducing parasitic capacitive coupling. The present invention includes three embodiments designed to reduce the high frequency interference pickup by the read element 610 of the magneto-recording head by reducing the capacitance of various head elements. In one embodiment, the area of the contact pads 610 is reduced. The contact pads 610 that connect to the GMR sensor are reduced to a minimal surface area, that in one embodiment is less than about 20 μm , and in a more preferred embodiment is about 10 μm . Preferably, the contact pads 610 are covered with photoresist and hard baked. The photoresist is left on as an insulator. The contact pads 610 are also preferably connected by studs 604 to an alumina undercoat 608 that rests on the substrate 614 from which the contact pads 610 are to be isolated in order to reduce parasitic capacitance. The studs 604 suspend the contact pads 610 through a small hole or "via" that is preferably filled with a conducting material. Copper is preferred. The suspension of the contact pads 610 allows the area of these contact pads 610 to be reduced, thus reducing parasitic capacitance coupling.

A second embodiment of the present invention is designed to reduce high frequency interference by increasing the separation between the contact pads 610 and the substrate material 614. One example of a manner of achieving a greater separation between the contact pads 610 and the substrate material 614 is to increase the thickness of the alumina undercoat 608. The layer of alumina undercoat 608 is deposited prior to the S1 layer 314 (seen in Figure 3). A thickness of between about 20 to about 30 microns is preferably deposited, whereas prior art thicknesses have been about 3.5 μm to about 5 μm . The alumina undercoat 608 preferably comprises Al_2O_3 , but may also comprise silicon oxide (SiO_2).

The thick layer of the alumina undercoat 608 increases the distance between the contact pads 610 and substrate material 614, which leads to a reduction in high frequency interference picked up by the read elements 610.

A third embodiment of the present invention comprises suspending the contact pads 610 on studs 604 as described previously, and using a material 602 having a low dielectric

constant as a spacer layer between the contact pads 610 and the substrate 614. Under this embodiment, the need to increase the thickness of the alumina undercoat 608 may be eliminated. An increase in the thickness of the alumina undercoat 608 is less preferred, as it may introduce stress in the film and create a delimitation from the substrate material 614. The low dielectric material 602 preferably has a dielectric constant less than about 10 and a more preferably dielectric constant of about 3. An example of a low dielectric material 602 placed as a spacer between the contact pads 610 and the substrate 614 comprises silicon dioxide, which has a dielectric constant of about 3. Figure 6 depicts a hard photoresist encapsulating the studs 604 and is used as a platform for the contact pads 610. The small area of the studs 604 leads to a small capacitance to the substrate 614, while the area of the contact pads 610 is separated from the substrate 614 by a low dielectric material 602, leading to a small overall capacitive coupling.

The present invention may be embodied in other specific forms without departing from its spirit or essential characteristics. The described embodiments are to be considered in all respects only as illustrative and not restrictive. The scope of the invention is, therefore, indicated by the appended claims rather than by the foregoing description. All changes which come within the meaning and range of equivalency of the claims are to be embraced within their scope.

What is claimed is: